REDUCTION OF KELVIN CHECK FAILURE OF DEVICE A AT QFN TEST Gimberlyne Joyce L. Barcarse

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ABSTRACT

Yield in semiconductor manufacturing is a critical metric, directly impacting production efficiency and costeffectiveness. During electrical testing, semiconductor devices undergo various assessments to ensure they meet specified electrical characteristics and performance requirements. Some devices will undergo the Kelvin Check Test, it is performed to measure and check the electrical contact resistance or connection between the test probes and the device under test (DUT).

Device A is a Quad Flat No-Lead (QFN) which undergoes rigorous testing procedures to ensure its electrical integrity and performance. However, Kelvin check Test failures during testing presents significant challenges, potentially compromising test accuracy and the efficiency of production.

This paper presents a Six Sigma approach to reduce Kelvin Check Test failures during testing of device A. Through the Define, Measure, Analyze, Improve, and Control (DMAIC) approach, critical parameters influencing Kelvin Check failures are identified, analyzed, and optimized. Statistical methods and process optimization techniques are applied to enhance test socket design, material selection, testing and setup procedures. Validation demonstrates a substantial reduction in Kelvin Check failures, leading to improved test yield and efficiency. Implementation of this Six Sigma methodology enables semiconductor manufacturers to achieve enhanced consistency, reduced testing costs, and improved quality assurance in QFN testing.

1.0 INTRODUCTION

1.1 Historical Background

The QFN Final Test process has historically been fundamental in ensuring product quality and operational efficiency. However, the device A is the top yield killer among devices posed a significant challenge from January 2022 to December 2022. The historical data analysis reveals that device A incurred a substantial scrap cost of \$179,115 during the specified period, underscoring its significance as the primary contributor to Overall QFN Final Test process yield degradation. Despite efforts to maintain a targeted Final Test Electrical Yield of 97.50%, the Kelvin Check emerged as the principal driver of failure and associated scrap costs, underscoring the necessity for a proactive approach to confront these challenges.

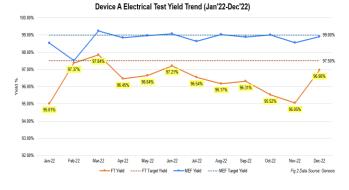


Fig 1 QFN Final Test – Electrical Test Yield Trend (Low Yield). Target yield of device A = 97.50%, target is not met.

1.2 Kelvin Check Test Fail

The term "Kelvin Check Test Failure" typically refers to a situation where the Kelvin Check, a type of test used in electronics manufacturing to verify the integrity of electrical connections, has produced results indicating a failure or anomaly. This failure could signify various issues such as improper contact between the test points as shown in Fig 2. and the device under test, electrical continuity problems, or deviations from specified parameters.

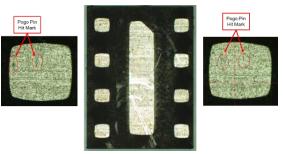


Fig 2. This is a sample unit of device contact pad that resulted to Kelvin Check Fail during Electrical Test using Pogo Pin (force and sense) Test Socket.

2. 0 REVIEW OF RELATED WORK

Not Applicable.

3.0 METHODOLOGY

3.1 Define Phase

Based on reject bin analysis, Top 1 Contributor comes from rejects of Electrical Rejects and streamlining on Electrical Rejects, 65% of rejects are from Parametric Rejects.

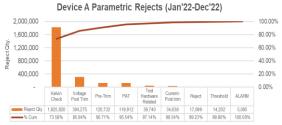


Fig. 3, Kelvin Check Failure is the Top 1 Contributor for Parametric Rejects.

The project target to reduce the defect PPM of Kelvin Check Failure is 16,334 PPM, aiming for a 30% reduction, PPM will be presumed to drop to 11,434 PPM per month.

3.2 Measure Phase

3.2.1 Process and Process Step Analysis

The SIPOC and Top chart show the three (3) sub-process critical to the occurrence of Kelvin Check Failure.

3.2.2 Tester Machine MSA

MSA was performed on the Pilot machine and other Tester on which these machines have the same version and are being used by the operation. Overall MSA in terms of BIAS and GR&R result passed wherein the tester is a reliable measurement system in terms of accuracy and precision. As a result, equipment is fit for use in detecting the occurrence of Kelvin Check Failure. The results were summarized as presented on below table:

KPIV / KPOV (Parameter)	Equipment	MSA Method	Test Method	Acceptability Criteria	Actual Result	Remark
		Bias (4V)	One-sample t Test	p-value > 0.05 or mean <permissible error<="" td=""><td>mean=0.00142</td><td>Pass</td></permissible>	mean=0.00142	Pass
		Bias (-4V)	One-sample t Test	p-value > 0.05 or mean <permissible error<="" td=""><td>0.5823 > 0.05</td><td>Pass</td></permissible>	0.5823 > 0.05	Pass
		Bias (10V)	One-sample t Test	p-value > 0.05 or mean <permissible error<="" td=""><td>mean=0.00019</td><td>Pass</td></permissible>	mean=0.00019	Pass
		Bias (-10V)	One-sample t Test	p-value > 0.05 or mean <permissible error<="" td=""><td>moan=-0.000142</td><td>Pass</td></permissible>	moan=-0.000142	Pass
		Bias (20V)	One-sample t Test	p-value > 0.05 or mean <permissible error<="" td=""><td>0.2920 > 0.05</td><td>Pass</td></permissible>	0.2920 > 0.05	Pass
Kelvin Check Failure	Tester	Bias (-20V)	One-sample t Test	p-value > 0.05 or mean <permissible error<="" td=""><td>mean=-0.00219</td><td>Pass</td></permissible>	mean=-0.00219	Pass
1 allure	(A & B)	Bias (36V)	One-sample t Test	p-value > 0.05 or mean <permissible error<="" td=""><td>mean=-0.070182</td><td>Pass</td></permissible>	mean=-0.070182	Pass
		Bias (-36V)	One-sample t Test	p-value > 0.05 or mean <permissible error<="" td=""><td>0.0744 > 0.05</td><td>Pass</td></permissible>	0.0744 > 0.05	Pass
		Bias (108V)	One-sample t Test	p-value > 0.05 or mean <permissible error<="" td=""><td>0.03451 > 0.05</td><td>Pass</td></permissible>	0.03451 > 0.05	Pass
		Bias (-108V)	One-sample t Test	p-value > 0.05 or mean <permissible error<="" td=""><td>0.1390 > 0.05</td><td>Pass</td></permissible>	0.1390 > 0.05	Pass
		0040	41010 0000000	%GR&R < 10%	0.33253% < 10%	Pass
		GR&R	ANOVA (Crossed)	ndc≥ 5	424 ≥ 5	Pass

Table 1 Overall MSA result of Tester machine.

3.3 Analyze Phase

3.3.1 Fishbone Diagram, Cause and Effect Analysis & Matrix

Thirty-five (35) probable root causes related to the occurrence of Kelvin Check Failure were identified and listed through Fishbone diagram and Cause and Effect Analysis Matrix. After scoring, prioritization, grouping and validation, Twelve (12) major root causes were known valid. (1) Unstable measurement and in good condition of Load Board (2)Broken/ Damaged Socket (3) Worn out Pogo Pins (4) Out of specs of device Pad Cutting (5) Misalign X and Y Precisor jaw (6) Misaligned Turret Pickup Head vs. device (7) High Contact Resistance on Pogo Pins (8) Incomplete and Wornout Screws (9) Insufficient Z-Axis Height and Misaligned X and, Y-axis Test Stand (10) Unoptimized Machine Parameter Setting (11) No Time limit of Ionizing of Lot (12) Dirty Canister

3.3.2 Potential root cause 1: Unstable measurement and in good condition of Load Board

Components on the load board, such as resistors, capacitors, or connectors, may degrade over time, affecting their performance and introducing instability in measurements. Despite the load board being physically intact, there could be issues with the contacts. Over time, contacts can degrade due to oxidation or wear and tear, leading to intermittent connections and unstable measurements. Load boards may vary responses causing failures on specific boards. This failure may lead to kelvin Check failures on specific boards.

3.3.2.1 Verification

Through actual checking of historical data of defective load board used during production that resulted to Kelvin Check Failure, there are cases of defective load board that was used during setup to production.

TEST#	RESULT	UNITS	LOWER	UPPER	ALARM	TEST NAME
			********			******************************
9000.0	10005		0	99999		Selected test mode
9001.0	4		0	7		Read test board ECD#
9002.0	4		0	7		Read test board BID#
9010.0	0.109	Ohm	0.025	2.000		Kelvin resistance of IN1 pin
9011.0	0.108	Ohm	0.025	2.000		Kelvin resistance of IN2 pin
9012.0	0.017	Ohm	0.025	2,000	FAIL	Kelvin resistance of OUT1 pir

Fig. 4, result of Kelvin Failure of the load board during setup isolation.

3.3.3 Potential root cause 2: Broken/ Damaged Socket

Test Socket involves connecting electronic components or devices to testing equipment for Testing purposes. These sockets contain spring-loaded pogo pins that make temporary electrical connections with the device under test (DUT) when it's inserted into the socket.

3.3.3.1 Validation on Good and damaged Socket through Chi-Square Test Hypothesis testing.

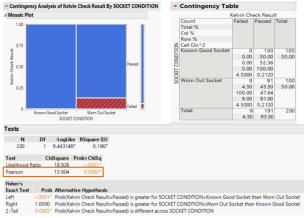


Fig. 5, The use of worn-out sockets is significantly different in using known good sockets and has significant variation. The use of worn-out sockets will result in Kelvin Check Failure.

3.3.4 Potential root cause 3: Worn out Pogo Pins

Pogo pins play a vital role in electronic testing by providing a convenient, efficient, and reliable means of making temporary electrical connections with the DUT. Their springloaded design, high contact force, and versatility make them essential components in testing. Over time, the repeated compressions and releases they undergo during testing can cause wear and tear on the spring mechanism and the contacting surface of the pin.

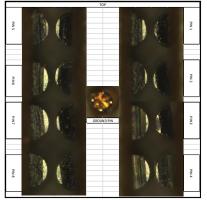


Fig. 6, Sample worn-out Pogo Pins

3.3.4.1 Validation on Good and Worn out Pogo Pins through Chi-Square Test Hypothesis testing.



Fig. 7, The use of worn-out pogo pins is significantly different in using known Good Pogo Pins and has significant variation. The use of worn-out pogo pins will result in Kelvin Check Failure.

3.3.5 Potential root cause 4: Out of specs of device Pad Cutting

A reliable package saw ensures uniform cutting across the entire wafer, resulting in consistent dimensions and quality of the individual QFN packages. This consistency is essential for accurate and reliable testing results.

3.3.5.1 Verification

Through actual dimension analysis on the historical data of Low Yield due to Kelvin Check Failure, there are cases of device Pad Cutting which are relax specs since 0 is the minimum specs criteria.

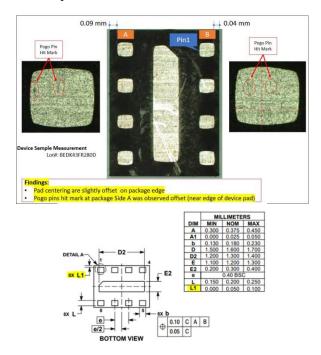


Fig. 8, Actual Dimensional Checking of device Pad Centering

3.3.6 Potential root cause 5: Misalign X and Y Precisor Jaw

Precisor Jaws or Rotor jaws securely hold the device or unit in place prior transferring to orientation table then to test site prior Electrical testing operations. This ensures stability and accuracy throughout the Test process, preventing movement that could compromise the Alignment of device prior going to testing site /socket. Any misaligned unit during testing is automatically tagged kelvin check failure during Testing as reject.

3.3.6.1 Verification

Through actual checking of historical data of mis-aligned X and Y precisor jaw used prior production or after Preventive Maintenance that resulted to Kelvin Check Failure.

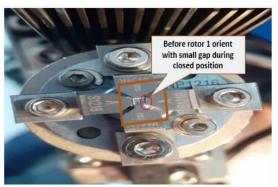


Fig. 9, Actual Misaligned Precisor Jaw

3.3.7 Potential root cause 6: Misaligned Turret Pickup Head vs. device

The Pick-Up Head (PUH) serves as the arm of a test and tape turret machine, responsible for lifting and transferring each unit sequentially throughout the machine until the testing and taping processes are completed.

3.3.7.1 Validation

Upon reviewing historical data, occurrences of misalignment between the Turret Pickup Head and the device have been identified through actual checks.



Fig. 10, Misaligned Turret Pickup Head vs. device A

3.3.8 Potential root cause 7: High Contact Resistance on Pogo Pins

High contact resistance on pogo pins occurs when there is difficulty in establishing a reliable electrical connection between the pins and the contact of device. This increased resistance can occur due to various factors such as corrosion, contamination, mechanical wear, or insufficient pressure exerted by the pogo pins during contact. High contact resistance can lead to unreliable electrical connections, signal degradation, or even complete failure of the system or device utilizing the pogo pins.

3.3.8.1 Validation on Good and Worn out Pogo Pins through Chi-Square Test Hypothesis testing.

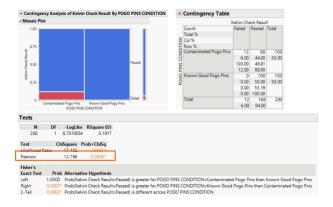


Fig. 11, The use of contaminated foreign material on Pogo Pin tips is significantly different in using known Good Pogo Pins and have significant variation. The use of contaminated foreign material on Pogo Pin will result in Kelvin Check Failure.

3.3.9 Potential root cause 8: Incomplete and Worn-out Screws

Incomplete screws refer to those that are not fully installed or tightened properly. This can happen due to human error during assembly or maintenance. Incomplete screws can result in loose connections, which may lead to vibrations, misalignment, or even disassembly of mechanical parts over time.

Worn-out screws occur when the threads or heads of the screws degrade due to friction, corrosion, or overuse.

3.3.9.1 Verification

After checking the historical data, instances of Kelvin check failures have been attributed to the use of incomplete and worn-out screws during production.

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STATUS 🛛	STATUS OWNER	COMMENTS		•
LSG REPAIR	156	OK- RE-CLEAN	SITE 2 DUE TO TEST HARDWARE > DONE REPAIR- CHECK SC SOCKET ON SITE 2 ED BY HW- SEEN INCOMPLETE SCREW ON SOCKET- REPLACED - OK RE- AUTO RAN PASSED STAT: RTP	
STATUS	✓ STATUS OW	NER	COMMENTS	ð
BUY OFF (OPERATOR VALIDATION OPERATIONA	L) PRODUCTIO	N	check socket at site 1_perform cleaning_remount socket seen incomplete screw_align and check contact_result consistent pass_for lot monitoring_machine endorse to production	

Fig. 12, Actual Machine Setup downtime for incomplete

3.3.10 Potential root cause 9: Insufficient Z-Axis Height and Misaligned X, Y and Z-axis Test Stand

The test stand's misaligned X, Y, and Z axes, along with insufficient Z-axis height, can lead to inaccuracies and failures in testing. If the Z-axis height is inadequate, it may prevent the test equipment from reaching or properly contacting the Test Socket or DUT. This limitation can hinder the testing process, leading to incomplete or inaccurate results and definitely can cause kelvin check failure.

3.3.9.1 Verification

After checking historical records, it has been found that Kelvin check failures during production were caused by a Test Stand with Misaligned X, Y, and Z axes and Insufficient Z-Axis Height.

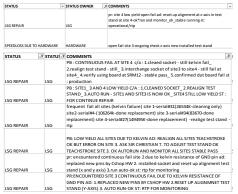


Fig. 13, Actual Machine Setup downtime for incomplete

3.3.11 Potential root cause 10: Unoptimized Machine Parameter Setting

Machine parameter settings that are not optimized can lead to various inefficiencies and issues in manufacturing processes especially in Testing.

3.3.11.1 Validation

Review historical data of unoptimized machine parameter settings on Test Force, Over Press and Over Travel using DOE to identify the height parameters significant to Kelvin Check Failure. Significant test result: Based on DOE, Test Stand Height and Over Travel are significant to the occurrence of Kelvin Check Failure rejects and the model is behaving linear.

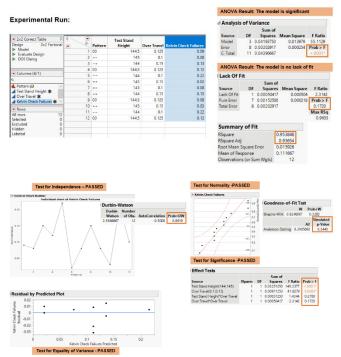


Fig. 14, DOE Result, The model is adequate and Passed the test based on the Statistical assumption result

3.3.12 Potential root cause 11: No Time limit of Ionizing of Lot

Ionizing is a process used in various industries, such as semiconductor manufacturing or pharmaceutical production, to neutralize static charges on materials or components. This helps prevent damage to sensitive electronic devices or ensure product quality and safety. When there's no time limit for ionizing a lot, it means the duration of exposure to ionization is not regulated and the adhesive on the device pads will not be removed.

3.3.12.1 Verification

Historically, there has been a persistent issue of low yield during the Testing process, primarily kelvin check failure due Insufficient time of ionizing of lot.

STATUS	Ŧ ŝ	STATU	Ŧ	COMMENTS	π.
				PB: OPEN FAIL SITE 1 AND 3 AD: REPLACED POGO PINS ON SITE1_CLEANED	2
				SCOKET OF TEST SITE3_BOTH REALIGNED TEST SITE (X-Y AXIS POSITION)_	
				AUTORUN THEN MONITORRED ST: RTP (CANISTER #2 IS SUBJECT FOR	
LSG REP	AL	LSG		IONIZING)	

Fig. 15, Actual Machine Setup downtime for Ionizing Concern

3.3.13 Potential root cause 12: Dirty Canister

A "dirty canister for QFN packages" refers to a container or holder used to store QFN (Quad Flat No-leads) semiconductor packages that has become contaminated or soiled. When the canister used to store QFN packages becomes dirty or contaminated, it means that it has accumulated dirt, dust, or other foreign particles. This contamination can potentially affect the cleanliness and integrity of the QFN packages stored inside.

3.3.13.1 Verification

A recurring challenge has been observed in the testing process, with low yield rates primarily attributed to Kelvin check failures resulting from a dirty canister.

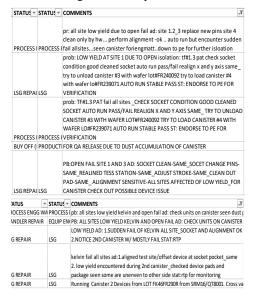


Fig. 16, Actual Machine Setup downtime for Dirty Canister

4.0 RESULTS AND DISCUSSION

4.1 Improve Phase

4.2 Unstable measurement and in good condition of Load Board: Inclusion of PASSED Data log reference of Load board prior issuance to Production.

Issuance to production means including a record that confirms the load board has successfully passed testing or inspection. This process guarantees that the load board adheres to necessary standards and specifications prior to its deployment in production. Additionally, data logs are stored in a system for future reference, ensuring the integrity of the recorded readings.



Fig. 17, Actual System that Saves Data logs

4.3 Broken/ Damaged Socket: Redesign socket

The previous design has a Unibody type and a risk of pogo pin rotation thus improvement of design was implemented into modular design which is more cost-efficient in terms of replacement and anti- rotation pogo pin was used. By implementing these redesign strategies, the test socket can be significantly improved in terms of durability, reliability, and resistance to damage, thereby enhancing its performance and longevity in testing applications.

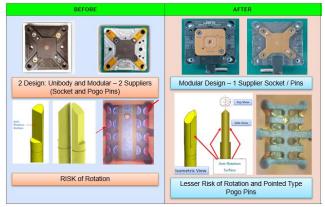
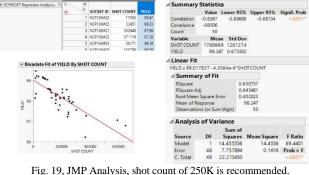


Fig. 18, GAP Analysis and comparison of the Socket and Pogo Pin Design

4.4 Worn out Pogo Pins: Established Pogo Pins Tool life thru Handler Shot Count Alarm

Set the Handler Shot count / Tool life based on Regression Analysis which is 250K and thus will be triggered once reach the shot count set on the Handler, it will prompt the operator to ask assistance to line sustaining personnel (LSG) for replacement and reset the alarm. By implementing a handler shot count alarm system, you can proactively monitor the health of pogo pins, minimize the risk of unexpected failures during testing operations, and prolong the lifespan of your automated testing equipment.



to achieve 97~97.5% Electrical Target Yield

4.5 Out of specs of device Pad Cutting: Improve the Frequency & Sample Size of QFN Package Singulation Measurement Procedure

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Existing Procedure for Non-Periodical Sampling is being done after Change of Operation Instruction only. Improving into after Change of Package is the new frequency and sample size of the QFN package singulation measurement procedure and implementing systematic enhancements, you can enhance product quality, minimize out-of-spec occurrences, and ensure the reliability of your manufacturing process.

4.6 Misaligned X and Y Precisor jaw, Misaligned Turret Pickup Head vs. device: Execution of Precisor Alignment Jig and Turret Alignment Jig during Set-up Conversion and PM

Enhance the regularity of conducting precisor jaw and turret pickup head alignment not solely during preventive maintenance (PM) but also throughout handler and setup conversion. By implementing these steps to execute precisor and turret alignment during setup conversion and PM, you can proficiently rectify misalignments, enhance equipment performance, and uphold the precision and dependability of the manufacturing operations.



Fig. 20, Pickup Head Calibration Procedure

4.7 High Contact Resistance on Pogo Pins: Installation of Inline Air-Blow cleaning of socket

To address high contact resistance on pogo pins, consider implementing inline air-blow cleaning for the socket. By installing inline air-blow cleaning for the socket pogo pins, high contact resistance on pogo pins as part of mitigation thus enhance overall reliability, and optimize the performance of your production line.



Fig. 21, Air Blow on Socket Pogo Pins

4.8 Incomplete and Worn-out Screws: Inclusion of Socket Crews as a Check Item of line sustaining personnel during the Setup/Repair buy-off

	9	Check DUT Name vs SO		Match Mismatch DN/A	
	10	Check Interface cable connection		□Match □Mismatch □N/A	
5	11	Carrier Tape Type: □3M □C-pak □Advantek □ENR	Description or Part Number:	Description or Part Number:	Description or Part Number:
REPAIR / SET	12	Cover Tape Type for SRM/UENO: ISM 2671A =180±5°c ISMmitomo Z7302 = 180±5°c IE&R F40R SP =160±5°c Cover Tape Type for TSCP1 (PICKER): IE&R -F40R SP = 170±5°c	Actual Temp: C	Actual Temp: C	Actual Temp: °C
R	13	Check Actual Carrier Tape vs SO	Match Mismatch N/A	□Match □Mismatch □N/A	⊡Match ⊡Mismatch ⊡N/A
	14	Check Actual Cover Tape vs SO	DMatch DMismatch DN/A	□Match □Mismatch □N/A	DMatch DMismatch DN/A
	15	PBFT: 40gF – 90gF	Pass DFail DN/A		
	16	Sealing Appearance	□Pass □Fail	□Pass □Fail	□Pass □Fail
	17	Check In-pocket Taping Orientation vs SO	□Match □Mismatc □N/A	EMatch EMismatch EN/A	Match DMismatch DN/A
	18	Conduct Open Socket Test to ALL Test Sites.	□ Pass □Fail □N/A		
	<u>19</u>	Check Actual Socket Screws	Complete Wom-out		
	2010	Stray unit Inspection on Test Site, Honner Feerler Rowl Linear	🗆 Na Hait 🗆 With Haitle		
		Fig. 22, Check It	ems and Setup	/Repair buy-of	f

4.9 Insufficient Z-Axis Height and Misaligned X and, Y-axis Test Stand: Redesign of Test Stand with fixed Z-Height and micrometer adjustment on X and Y-axis.

To address the issues of insufficient Z-axis height and misaligned X and Y-axis on the test stand, consider redesigning the test stand with fixed Z-height and micrometer adjustments on the X and Y-axis. By redesigning the test stand with fixed Z-height and micrometer adjustments on the X and Y-axis, you can effectively address issues of insufficient height and misalignment, resulting in improved accuracy, reliability, and efficiency in your testing processes.

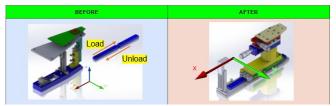


Fig. 23, GAP Analysis and comparison of the Socket and Pogo Pin Design

4.10 Utilizing a DOE method employing a 2x2 factorial design for optimizing test stand height and overtravel settings enables the systematic identification of the most impactful factors and their ideal levels. This approach promotes improved effectiveness and efficiency throughout your testing protocols. To prevent unauthorized modifications, the overtravel setting was configured on machine settings to include a high level secured by password protection.

Source Test Stand H Over Travel(I			lorth 1.852 1.650		PValue 0.00000 0.00022							
Bernovs Ad	ld Edit	Undo D FDR										
Lack Of Fi	t				a • Predictio	n Profiler						
Source Lack Of Fit Pure Error Total Error	7	Sum of Squares 0.00081667 0.00152500 0.00234167	Mean Square 0.000408 0.000218	F Ratio 1.8743 Prob > F 0.2229 Max RSq 0.9653	River Once Salves 19100-1000 8	0.2 0.15 0.05 0 1 0.75				A M	/	
Summar	y of	Fit			Approx.920867	0.5						
RSquare RSquare Ad Root Mean Mean of Re Observation	Squar spons	e	0.94674 0.934904 0.01613 0.111667 12		٥	00	range 145 Test Stand Height		1 2 3 0.15	0.15	ST S	- gg =

Fig. 24 Based on the profiler of the refined model with predictive capability of 94% the best parameter combination to be used to achieve maximum desirability are, Over Travel= 0.15 mm & Stand height = 145.

	Gap (mm)	OverTravel (mm)	OvesPiess (mm)	(pube)	OverPress (pulse)	TestForce [g]
SP1 - Singulator	0.1	0	9	-1600	0	500
SP2-R Piecisor	0.05	0	0	-800	0	500
SP3 - Vision Table	0.12	0	0	-1920	0	500
SP4 - Rotor Oner#	0.05	0	0	-800	0	500
SP5 - Test Site 1	0	0.15	0.1	2400	1600	1000
SP6 - Test Site 2	0	0.15	0.1	2400	1600	1000
SP7 - Test Site 3	0	0.15	0.1	2400	1600	1000
SP8 - Test Site 4	8	0.15	0.1	2400	1600	1000

Fig. 24. Machine Setting on Over Travel

4.11 No Time limit of Ionizing of Lot and Dirty Canister: Automated Ionizing

Through the transition from manual ionizing to automated ionizing, greater control and efficiency can be introduced into the ionization process. This shift also eliminates the risk of prolonged exposure due to the absence of a time limit, while enhancing overall cleanliness and quality control throughout the production line.



Fig. 25, Manual ionizing to Automated ionizing

4.12 Before and After Performance Comparison after Pilot run

Upon initiating the implementation of CAPAs to address the Kelvin Check Failure of device A during QFN testing, notable advancements were achieved. Within a span of three months, the ppm level fell below the baseline, successfully meeting the target of 11,434 ppm, with the actual count recorded at 4,844 ppm.

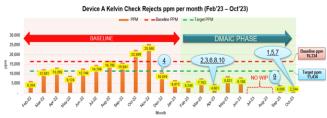


Fig. 26, Performance of Machine after completing all actions.

4.13 Control Phase

All actions and controls were documented and implemented. Furthermore, the PFMEA & Control Plan underwent a thorough review and alignment with the project. Additionally, a Project Transition Plan for Sign of Black Belt has been developed following the review process.

The project has yielded actual cost savings of 499 USD, meeting the goal of reducing Kelvin Check Failure of device A at QFN Test by at least 30%, from 16,334 PPM to 11,434 PPM. The projected annual cost savings amount to 5,990 USD.

5.0 CONCLUSION

In conclusion, to address the objective of reducing Kelvin Check Failures of device A, a comprehensive approach was adopted. This included the implementation of Corrective and Preventive Actions (CAPAs) chosen from the valid Key Process Input Variables (KPIVs). Additionally, various measures were enacted, such as integrating into the system the PASSED data log references for load boards, redesigning sockets, establishing monitoring for pogo pins tool life, enhancing frequency and sample size in QFN package singulation measurements, executing precisor and turret alignment jigs during setup and maintenance, installing inline air-blow cleaning for sockets, Check Item enhancement of line sustaining personnel during the buy-off during Setup/Repair, redesigning of Test Stand with fix Z-Height and micrometer adjustment on X and Y-axis, optimizing test stand height and overtravel through a Design of Experiments (DOE), and transitioning from manual to automated ionizing of lots.

6.0 RECOMMENDATIONS

In light of the validated impact, this technical paper proposes assessing the potential applicability of the implemented measures to alternative machines and packages.

7.0 ACKNOWLEDGMENT

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Lastly, heartfelt appreciation is extended to all the team members involved in this project, whose selfless dedication and time contributed significantly to its success.

8.0 REFERENCES

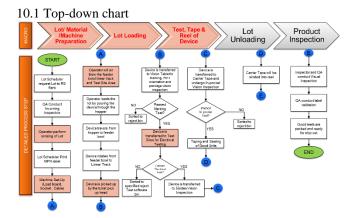
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9.0 ABOUT THE AUTHORS



Gimberlyne Joyce L. Barcarse holds the position of Equipment Engineer in the Final Test Department at Onsemi, six years of tenure with the company. She graduated with a degree in Mechatronics Engineering.

10.0 APPENDIX



10.2 Fishbone Diagram

